

Errata for Optimal Control for Chemical Engineers

Page xvi, line 9

$$y'' \equiv \frac{dy'}{dx} \equiv \frac{d^2 y}{dx^2}$$

Page 1, line 9 “An optimal control is a function that optimizes ...”

Page 7

$$I = y(L) = y(0) + \int_{y(0)}^{y(L)} dy = y_0 + \int_0^L \frac{dy}{dz} dz \quad (1.12)$$

Page 8

$$\frac{\partial T}{\partial t} = -v \frac{\partial T}{\partial z} + \frac{h}{\rho C_p} [T_w(t) - T] \quad (1.13)$$

Page 9

$$\frac{dT_s}{dz} = \frac{h}{v\rho C_p} [\theta - T_s] \quad (1.15)$$

Page 12, Figure 1.7 Replace the labels “monomer:” and “polymer:” by “initiator:” and “monomer:”, respectively.

Page 39, line 9,11

$$I(y_0 + \alpha h) = I(y) = \frac{\alpha h_1 h_2}{h_1 + h_2}$$

$$\delta I(y_0; h) = \frac{d}{d\alpha} I(y_0 + \alpha h)_{\alpha=0} = \frac{h_1 h_2}{h_1 + h_2}$$

Page 41, line 3

- δy and $\delta y'$ are the functions $h(x)$ and $h'(x)$, respectively.

Page 41, last sentence of Example 2.9 “Upon substituting $\delta y = -x$ and the corresponding ...”

Page 66

$$\frac{\partial H}{\partial \lambda} \equiv H_\lambda = \dot{y} \quad (3.28)$$

$$\frac{\partial H}{\partial y} \equiv H_y = -\dot{\lambda} \quad (3.29)$$

$$\frac{\partial H}{\partial u} \equiv H_u = 0 \quad (3.30)$$

Page 67, line 6

1. the state equation, Equation (3.25), obtained from $\dot{x} = H_\lambda$ and the initial condition $x(0) = 0$;

Page 67, 2nd last equation

$$J = \int_0^{t_f} \left(F + \sum_{i=1}^n \lambda_i G_i \right) dt \equiv \int_0^{t_f} f(\mathbf{y}, \dot{\mathbf{y}}, \mathbf{u}, \boldsymbol{\lambda}) dt$$

Page 90, the line before Equation (4.2) Remove the extra “the” before “constraint $K(y) = k_0, \dots$ ”

Page 101, the equation before Equation (4.13)

$$\delta K_i = \lim_{\Delta t_i \rightarrow 0} \left[-\frac{\delta y_{i+1} - \delta y_i}{\Delta t_i} + \underbrace{g_y|_{t_i} \delta y_i + g_u|_{t_i} \delta u_i}_{\delta g_i} \right] \Delta t_i$$

Page 103, 2nd last line of Example 4.3 “exists at least one set of variations $(\delta \dot{\mathbf{x}}, \delta \mathbf{x}, \delta u)$ at each $t \dots$ ”

Page 106, line 13–17 For consistency, use μ instead of ν as follows:

$$M(\hat{\mathbf{y}}, \mathbf{u}) = J(\hat{\mathbf{y}}, \mathbf{u}) + \int_0^{t_f} \sum_{i=1}^l \mu_i h_i(\hat{\mathbf{y}}, \mathbf{u}) dt = J + \int_0^{t_f} \boldsymbol{\mu}^\top \mathbf{h}(\hat{\mathbf{y}}, \mathbf{u}) dt$$

where $\hat{\mathbf{y}}$ denotes the state vector that satisfies state equations for any admissible control vector \mathbf{u} and $\boldsymbol{\mu}$ is the vector of time dependent Lagrange multipliers

$$[\mu_1(t) \quad \mu_2(t) \quad \dots \quad \mu_l(t)]^\top$$

Page 108, line 12

$$J[\hat{u}(k_0 + \Delta k_0)] = J[\hat{u}(k_0)] + dJ[\hat{u}(k_0); \hat{u}_{k_0} \Delta k_0] + dJ[\hat{u}(k_0); \epsilon] + \epsilon_1(\Delta k_0 \delta u)$$

Page 111, 2nd last line

$$\mu \geq 0, \quad \underbrace{\mu(\hat{u} - c\hat{y})}_{\text{complementary slackness condition}} = 0 \quad \text{at} \quad t_f$$

Page 114, line 9

$$M = J + \int_0^{t_f} \left\{ \underbrace{\mu_1 \left[\frac{x_2}{x_1} - a \left(\frac{1}{b^{u_2 - c}} - 1 \right) \right]}_{K_1} + \underbrace{\mu_2(-u_2 + u_{\min})}_{K_2} + \underbrace{\mu_3(u_2 - u_{\max})}_{K_3} \right\} dt$$

Page 124, line 16

$$= \int_0^{t_f} (H_y + \dot{\lambda}) \delta y dt - \left[\lambda \delta y \right]_0^{t_f} + \int_0^{t_f} H_u \delta u dt + \int_0^{t_f} (-\dot{y} + H_{\lambda}) \delta \lambda dt$$

Page 154, line 14,15 Sum the terms containing δu_i separately as follows:

$$\delta J = \int_0^{t_f} \left[\sum_{i=1}^n \left(\frac{\partial H}{\partial y_i} \delta y_i + \frac{\partial H}{\partial \lambda_i} \delta \lambda_i - \lambda_i \delta \dot{y}_i - \dot{y}_i \delta \lambda_i \right) \right] dt + \int_0^{t_f} \left[\sum_{i=1}^m \frac{\partial H}{\partial u_i} \delta u_i \right] dt + \left[H - \boldsymbol{\lambda}^\top \dot{\mathbf{y}} \right]_{t_f} \delta t_f$$

Page 158, the equation after Equation (6.11)

$$\boldsymbol{\mu} = \begin{bmatrix} \mu_1 & \mu_2 & \dots & \mu_l \end{bmatrix}^\top$$

Page 160, 3rd equation

$$\begin{bmatrix} \dot{\lambda}_1 \\ \dot{\lambda}_2 \\ \dot{\lambda}_3 \end{bmatrix} = - \underbrace{\begin{bmatrix} 2(\lambda_1 - \lambda_2)a_1y_1e^{E_1/T} \\ (1 + \lambda_2 - \lambda_3)a_2e^{E_2/T} \\ (-1 + \lambda_3)a_3e^{E_3/T} \end{bmatrix}}_{-H_{\mathbf{y}}}$$

Page 166, line 8 Remove explicit t from the arguments as follows:

$$f_i(\mathbf{y}, \mathbf{u}) \leq 0, \quad i = 1, 2, \dots, l \quad \text{or} \quad \mathbf{f}(\mathbf{y}, \mathbf{u}) \leq \mathbf{0}$$

Page 167, last equation

$$\begin{bmatrix} \dot{\lambda}_1 \\ \dot{\lambda}_2 \\ \dot{\lambda}_3 \end{bmatrix} = - \underbrace{\begin{bmatrix} 2(\lambda_1 - \lambda_2)a_1y_1e^{E_1/T} \\ (1 + \lambda_2 - \lambda_3)a_2e^{E_2/T} \\ (-1 + \lambda_3)a_3e^{E_3/T} \end{bmatrix}}_{-L_{\mathbf{y}}}, \quad \begin{bmatrix} \lambda_1 \\ \lambda_2 \\ \lambda_3 \end{bmatrix}_{t_f} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

Page 168, last equation of Example 6.9 Remove the subscript $t = 0$ as follows:

$$\begin{bmatrix} \mu_1 \\ \mu_2 \end{bmatrix} \geq \begin{bmatrix} 0 \\ 0 \end{bmatrix} \quad \text{and} \quad \begin{bmatrix} \mu_1 \\ \mu_2 \end{bmatrix}^\top \underbrace{\begin{bmatrix} -T + T_{\min} \\ T - T_{\max} \end{bmatrix}}_{L_{\boldsymbol{\mu}}} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

Page 169, 1st equation Remove explicit t from the argument as follows:

$$\int_0^{t_f} F_i(\mathbf{y}, \mathbf{u}) dt = k_i, \quad i = 1, 2, \dots, l$$

Page 170, Example 6.10 For consistency, use $(y - y^*)$ instead of $(y^* - y)$.

Page 176, 3rd equation from bottom

$$H_u = 1 + \lambda_1 = 0$$

Page 177, 2nd equation

$$\begin{bmatrix} \lambda_1 \\ \lambda_2 \\ \lambda_3 \\ \lambda_4 \end{bmatrix}_{t_1-} = \begin{bmatrix} \lambda_1 \\ \lambda_2 \\ \lambda_3 \\ \lambda_4 \end{bmatrix}_{t_1+} + \underbrace{\begin{bmatrix} \frac{\partial q_1}{\partial y_1} & \frac{\partial q_1}{\partial y_2} & \frac{\partial q_1}{\partial y_3} & \frac{\partial q_1}{\partial y_4} \\ \frac{\partial q_2}{\partial y_1} & \frac{\partial q_2}{\partial y_2} & \frac{\partial q_2}{\partial y_3} & \frac{\partial q_2}{\partial y_4} \end{bmatrix}}_{\mathbf{q}_{\mathbf{y}}(t_1)}^{\top} \begin{bmatrix} \mu_1 \\ \mu_2 \end{bmatrix}$$

Page 178, Example of Section 6.7 For notational consistency in case of partial time derivatives, use c_t , δc_t , λ_t and $\delta \lambda_t$ instead of \dot{c} , $\delta \dot{c}$, $\dot{\lambda}$ and $\delta \dot{\lambda}$, respectively.

Page 182

$$\lambda_z(L, t) = 0, \quad 0 \leq t \leq t_f \quad (6.26)$$

Page 182, 1st item of Bibliography

K.J. Arrow, L. Hurwicz, and H. Uzawa. Constraint qualifications in nonlinear programming. *Nav. Res. Logist. Q.*, 8(2), 1961.

Page 204, 2nd and 3rd equations

$$\begin{aligned} \boldsymbol{\lambda}^{\top}(1) &= \begin{bmatrix} \lambda_1 \\ \lambda_2 \\ \lambda_3 \\ \lambda_4 \end{bmatrix}^{\top} = \underbrace{\begin{bmatrix} y_4 - b_1 y_2 \\ y_4 - b_2 y_3 \end{bmatrix}}_{\mathbf{q}^{\top}}^{\top} \underbrace{\begin{bmatrix} \alpha^r & 0 \\ 0 & \alpha^r \end{bmatrix}}_{\mathbf{W}} \underbrace{\begin{bmatrix} 0 & -b_1 & 0 & 1 \\ 0 & 0 & -b_2 & 1 \end{bmatrix}}_{\mathbf{q}_{\mathbf{y}}(1)} \\ &= \alpha^r \begin{bmatrix} 0 \\ -b_1(y_4 - b_1 y_2) \\ -b_2(y_4 - b_2 y_3) \\ 2y_4 - b_1 y_2 - b_2 y_3 \end{bmatrix}^{\top} \end{aligned}$$

Page 208, line 1,2 “and the final costates, $\lambda_4(1) = 0$ and”

$$\begin{bmatrix} \lambda_1 \\ \lambda_2 \\ \lambda_3 \end{bmatrix}_{\sigma=1}^{\top} = \underbrace{\begin{bmatrix} y_1 - y_{1,f} \\ y_2 - y_{2,f} \\ y_3 - y_{3,f} \end{bmatrix}_{\sigma=1}}_{\mathbf{q}^{\top}} \underbrace{\begin{bmatrix} \alpha^r & 0 & 0 \\ 0 & \alpha^r & 0 \\ 0 & 0 & \alpha^r \end{bmatrix}}_{\mathbf{W}} = \alpha^r \begin{bmatrix} y_1 - y_{1,f} \\ y_2 - y_{2,f} \\ y_3 - y_{3,f} \end{bmatrix}_{\sigma=1}^{\top}$$

Page 212, line 15,16 “... the optimal objective functional was -4.46 , which corresponds to the final product concentration of 4.46 g/cm^3 .”

Page 215, 3rd line from bottom “increased from 60 to 64.1 min .”

Page 219, 2nd last paragraph, line 4,5 “... the value of E was 4.0×10^{-7} .”

Page 227, 1st two equations

$$\begin{aligned} \frac{dy_{\lambda_0}}{dt} &= - \left[\frac{\lambda(y - y_f)}{2} + u_s \right] y_{\lambda_0} + \left[(y - y_f)\lambda_{\lambda_0} + \lambda y_{\lambda_0} \right] \frac{(y_f - y)}{2} - 2ky_{\lambda_0} \\ \frac{d\lambda_{\lambda_0}}{dt} &= -2y_{\lambda_0} + \left[\frac{\lambda(y - y_f)}{2} + u_s + 2ky \right] \lambda_{\lambda_0} + \left[(y - y_f)\lambda_{\lambda_0} + (\lambda + 4k)y_{\lambda_0} \right] \frac{\lambda}{2} \end{aligned}$$

Page 227, 3rd line after Results “shows the initial and optimal states and controls. The convergence ...”

Page 232, Exercise 7.3, 1st and 3rd equations

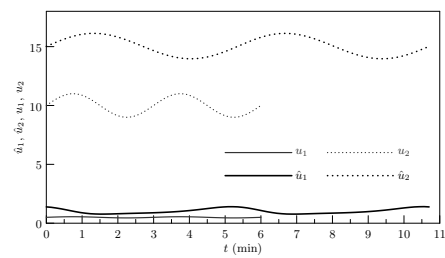
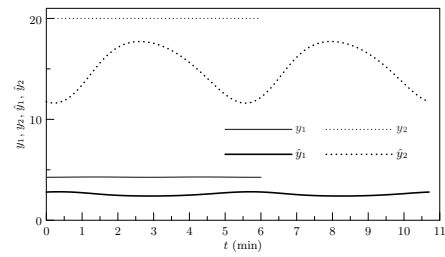
$$\begin{aligned} \frac{dy_1}{dt} &= -2y_1 - a_1 + (y_2 + a_1) \exp\left(\frac{a_2 y_1}{y_1 + 4a_1}\right) - (y_1 + 0.5a_1)u, \quad y_1(0) = y_{1,0} \\ I &= \int_0^{t_f} (y_1^2 + y_2^2 + a_3 u^2) dt \end{aligned}$$

Page 242, the equation before Equation (8.3)

$$\begin{bmatrix} H_{u_1} \\ H_{u_2} \end{bmatrix} = \tau \begin{bmatrix} \lambda_1(y_f - y_1) - \lambda_2 y_2 \\ \lambda_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

Page 246, Table 8.1 y_f is 3.56 g/cm^3 and k_0 is $10^{-2} (\text{cm}^3/\text{g})^2/\text{min}$.

Page 247, Figures 8.1 and 8.2



Page 247, 3rd line from bottom "... production rate of $7.8 \times 10^{-2} \text{ g}/(\text{cm}^3 \cdot \text{min})$."

Page 247, last line to the 1st line of next page "... maximized the average production rate to $0.17 \text{ g}/(\text{cm}^3 \cdot \text{min})$."

Page 248, Figure 8.3

